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Adsorption Kinetics and Isotherms for Removal of Rhodamine B (dye) using Adsorbents prepared from drinking water treatment sludge

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ABSTRACT

The present work aims to investigate the removal of Rhodamine B dye (RB) from aqueous solution by using adsorbents prepared from alum sludge (AS) and Mud sludge (MS) of drinking water treatment plant. The effect of dye concentration, contact time, pH, temperature and adsorbent dose on the dye removal was studied. The equilibrium adsorption data of RB dye on the developed adsorbents were analyzed by the Langmuir, Freundlich, Temkin and Dubinin-Radushkevich (D-R) Isotherms. The sorption data fitted well to Langmuir isotherm model. The maximum dye removal efficiency was observed at pH 7, contact time 90 min, and 0.1-0.25 gm dosage for both (AS) and (MS) adsorbents. Also, four kinetic models such as Pseudo-first order, Pseudo-second order, Intraparticle diffusion and Elovich models were tested to interpret the experimental data. The kinetic experimental data were fitted well to Pseudo-second order model. The thermodynamics parameters of adsorption system indicated spontaneous and endothermic process. Results indicate the effectiveness of the developed adsorbents for removing RB dye.

Key words:

Sewage sludge, Rhodamine B, adsorption, pollution, wastewater.

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Introduction

Dyes are chemicals that may be harmful and on binding with a material will give color to them. New dyes are synthesized and have several applications as they are gorgeously colorful. Textile is one of those industries where more and more dyes and pigments are used to color the products. In recent years, it is estimated that more than 100,000 dyes are available commercially (Lee and Choi, 2006) and their global production exceeds 800,000 tons per year (Bouasla et al., 2010). The colored dye effluents are generally considered to be highly toxic to the aquatic system. Some dyes are reported to cause skin irritation, dermatitis, allergy and cancer in humans (Salleh, et al., 2011).

Industrial wastewater, contain dyes, is usually treated by physical and chemical methods such as sonochemical degradation (Abbasi and ASI, 2008), photochemical degradation (Gupta et al., 2007), electrochemical degradation (Fan et al., 2008), coagulation and flocculation (Zonoozi et al., 2009), membrane separation (Sachdeva and Kumar, 2009), activated carbon adsorption (Tan et al., 2008) and oxidation or ozonation (Malik and Saha, 2003). However, in developing countries, these methods are still too expensive to be used widely. Developing economical adsorbents for dye treatment of industrial wastewater has attracted a great interest in recent years. Recently, the application of low-cost adsorbents for the dye removal has been reviewed (Bhatnagar and Sillanpaa, 2010).

Rhodamine-B (RB) is one of the water soluble xanthenes class dyes, a basic red cationic dye which is a common water tracer fluorescent. It is often used in textile, silk, wool, cotton, and food industries. It is potentially harmful to humans as it can cause eye burn, irritation to the skin, gastrointestinal and the respiratory tracts. For these reasons, the treatment of dye effluents is essential prior to their discharge into the receiving water bodies (Arivoli and Thenkuzhali, 2009).

The cost is actually an important parameter for comparison and selection of adsorbents. The literature survey reveals that there has been numerous researchs reported the using of low cost adsorbents for dye removal, which are economical viable, easily available, highly

effective in the adsorption process (Chamargore et al., 2010). Low-cost adsorbents have been studied for the removal of dyes and heavy metals from wastewater such as waste apricot (Sun and Yang, 2003), coconut shell (Kumar and Porkodi, 2007), dairy sludge (Gong et al., 2005), bamboo grass treated with concentrated sulfuric acid (Sumanjit and Prasad, 2001), peat (Sumanjit et al., 2010), bamboo (Ma et al., 2010), jack fruit peels (Jai and Jayaram, 2007), pistachio nut shells (Vijayalakshmi et al., 2011), date stone and palm tree waste (Belala et al., 2011), treated sewage sludge (Rashed et al., 2011), and phosphate slime (Rashed et al., 2015).

Alum and mud sludges are by-product from the processing of drinking water in drinking water treatment plants. Alum sludge produced when alum (aluminium sulfate) is used as coagulant. Mud sludge also by-product but when the quality of raw water is high and not needs to alum. The disposal of these sludge to a landfill environmental problems; since alum sludge contains a high level of aluminium, which has been shown to be toxic to aquatic life and relatively inert, providing marginal benefits to soil fertility. Moreover, the reuse of alum and mud sludge will be economically and environmentally beneficial.

Researches have shown that drinking water treatment sludge (Alum sludge) can be used as an effective adsorbent for phosphate (Yang et al., 2006; Al-Fatlawi and Neamah, 2015), and some heavy metals (Zhou and Haynes, 2010; Lee et al., 2006) but no researches has discussed its use as a Rhodamine-B dye adsorbent. It is noted from the literature that alum or mud sludge adsorbents has not investigated for Rhodamine-B dye removal.

The purpose of this study is to investigate the adsorption behavior of alum and mud sludge adsorbents for Rhodamine-B dye removal from polluted solution. The adsorption equilibrium, kinetics, isotherms, and thermodynamics studies were then studied to observe the effects of various process parameters such as initial dye concentrations, contact time, pH, dose, and temperature on Rhodamine-B dye removal.

2. Materials and methods

2.1. Sample collection.

Alum sludge and mud sludge were used as raw materials for preparation of adsorbent in the study. Mud sludge was obtained from Gabal Takok drinking water treatment plant at Aswan City, while Alum sludge was obtained from Fatera drinking water treatment plant at Kom Ombo city, Aswan governorate, Egypt. The sludge samples were air dried in a clean place and crashed into uniform 0.2 mm size, then oven dried at 105°C for 24h, cooled, and kept in the desiccators until used. The physico-chemical characteristics of Alum and Mud sludge are summarized in Table (1).

2.2. Preparation of Sludge (Alum and Mud) Adsorbents by Physical Activation:

Alum and mud adsorbents were obtained by physical and chemical activation as described previously in our published paper (Rashed et al. 2016). Based on the previous study, in physical activation of alum and mud sludge, 100 gm of dry sludge was pyrolyzed at 400, 500, 600, 700, 800, and 900° C for one hour. The resulted adsorbents are AS400, AS500, AS600, AS700, AS800, and AS900 for alum sludge adsorbent, and MS400, MS500, MS600, MS700, MS800, and MS900 for mud sludge adsorbent.

2.3. Preparation of Sludge (Alum and Mud) Adsorbents by Chemical Activation:

Chemical activation of alum and mud sludges were preceded by three methods as described in our published paper (Rashed et al. 2016) as follows:

2.3.1 Activation with Acetic Acid (CH_3COOH)

10 gm of dry sludge was mixed with 100 ml of each acetic acid concentration (0.1, 0.5, 1, 2 and 3 M), stirred at 60° C for four hours, filtered, washed with deionized water, and dried at 120° C for 12 hours. The dried residue was pyrolyzed in the oven at 500°C for two hours, and left in the desiccators for further use. The developed alum sludge adsorbents labeled AS1 (0.5 M AA), AS1(1 M AA), AS1(2M AA) and AS1(3M AA) for treatment with 0.1, 0.5, 1, 2 and 3 M acetic acid, respectively. The developed mud sludge adsorbents labeled MS1 (0.1 M AA), MS1(0.5 M AA), MS1(1 M AA) and MS1(2 M AA) and MS1(3 M AA) for treatment with 0.1, 0.5, 1, 2 and 3 M acetic acid, respectively(Rashed et al., 2016).

2.3.2. Activation of Alum and Mud Sludge with Acetic Acid followed by pyrolysis.

Sludge sample was mixed with water to yield the moisture content of 20%. The sludge pellet form was made by cutting it to a uniform size of 2-2.5 mm. Pellets were heated in an oven at 500° C for 2 hours. Pellets (10 gm) was mixed with 100 ml of each acetic acid concentration (0.1, 0.5, 1, 2, and 2M) and stirred at 60° C for 4 h. The sample was dried at 120° C for 12 hours, after that left in desiccators for use. The developed alum sludge adsorbents labeled AS2 (0.1M AA), AS2(0.5 M AA), AS2(1 M AA), AS2 (2M AA) and AS2 (3M AA) for treatment with 0.1, 0.5, 1, 2 and 3 M acetic acid, respectively. The developed mud sludge adsorbents labeled MS2 (0.1M AA), MS2(0.5 M AA), MS2 (1 M AA), MS2 (2M AA) and MS2 (3M AA) for treatment with 0.1, 0.5, 1, 2 and 3 M acetic acid, respectively(Rashed et al., 2016).

2.3.3. Activation of Alum and Mud Sludge with Nitric Acid

The dried sludge sample 10 gm was mixed with 50 ml of each HNO_3 concentrations (0.25, 0.5, 1, and 2 M), filtered and left for 24 hours. After that it washed with deionized water, dried at 60 °C in an oven for 24 h and left in desiccators for further use. The developed alum sludge adsorbents labeled AS3 (0.25M NA), AS3 (0.5 M NA), AS3(1 M NA) and AS3(2M NA) for treatment with 0.25, 0.5, 1 and 2 M nitric acid, respectively. The developed mud sludge adsorbents labeled MS3 (0.25M NA), MS3(0.5 M NA), MS3(1 M NA) and MS3(2M NA) for treatment with 0.25, 0.5, 1 and 2 M HNO_3 , respectively.

All the developed adsorbents were ground in an agate mortar and sieved to particle size 63 μm . The resulted adsorbents were successfully characterized by XRF, XRD, and SEM as mentioned previously in our published paper (Rashed et al.2016).

3. Analytical Measurement

The initial and residual Rhodamine-B dye concentration in the aqueous solution was analyzed using UV-Vis spectrophotometer (model Thermo Scientific Nicolet evolution 100).

Table (1). The physico-chemical characteristics of Alum and Mud sludge.

Properties	Alum Sludge	Mud Sludge
Moisture content %	10.95	9.86
Ash %	6.88	5.85
Volatile matter %	5.5	5.33
Matter soluble in water %	0.81	0.56
Matter soluble in 0.25 M HCl %	3.09	2.9
Bulk density, gmL ⁻¹	0.142	0.139
Specific gravity	1.009	1.004

Table (2). Removal percent of Rhodamine B by chemically activated adsorbents (AS &MS) using acetic acid and acetic acid with pyrolysis at 500 ° C

Activation by acetic acid (AA) and pyrolysis			Activation by acetic acid	
AA Concentration (M)	AS	MS	AS	MS
	Removal%	Removal%	Removal%	Removal%
0.1	48.9	69.6	80.6	72.9
0.5	50.8	58.6	70.2	77.8
1	57.4	55.2	69.8	62.2
2	65.5	52.7	60.2	54.6
3	72.2	49.6	51.3	45.4

Table (3). Removal percent of Rhodamine B by chemically activated adsorbents (AS &MS) with nitric acid .

Activation by nitric acid (NA)		
NA Concentration (M)	AS	MS
	Removal%	Removal%
0.25	95.2	92
0.5	83.5	78.6
1	75.4	72.9
2	64.23	58.7

Table (4). Removal percent of Rhodamine B by physically activated adsorbents (AS &MS).

Physically activated sludge		
Activator °C	AS	MS
	Removal%	Removal%
400	58.5	54.9
500	60.9	58.6
600	66.1	60.2
700	87.8	83.7
800	55.7	50.8
900	50.33	47.9

Table (5): Removal percentage (%) of RB dye on alum and mud sludge adsorbents according to initial RB dye concentration.

RhB Con. (ppm)	AS adsorbent				MS Adsorbent			
	AS1	AS2	AS3	AS700	MS1	MS2	MS3	MS700
50	73.09	81.78	94.57	88.9	69.55	77.58	90.45	84.23
60	69.72	75.1	84.1	78.1	60.2	69.81	82.5	75.8
70	61.7	65.4	72.3	70	55.29	62.33	69.5	66.9
100	50.5	54.8	62.1	58	47.2	52.3	60.2	56.14

Table 6. Results of isotherm plots for adsorption of Rhodamine B dye onto Alum and Mud Sludge Adsorbents.

Parameters	AS1	AS2	AS3	AS4	MS1	MS2	MS3	MS4
Langmuir Isotherm model								
Q ₀	23.365	24.096	25.641	24.69	22.727	23.697	25.707	27.55
b _L (L/mg)	0.131	0.203	0.4722	0.307	0.0859	0.1461	0.3473	0.1464
R ²	0.9995	0.9979	0.9929	0.9963	0.988	0.9973	0.9962	0.9854
Freundlich Isotherm model								
1/n	0.239	0.1805	0.0965	0.1346	0.257	0.2098	0.138	0.1692
K _f (mg ^{-1/n} L ^{1/n} g ⁻¹)	8.113	10.995	16.765	13.804	6.707	9.262	14.421	11.74
R ²	0.9517	0.9976	0.8874	0.9438	0.9411	0.9939	0.9832	0.9895
Temkin Isotherm model								
B (j/mol)	4.1589	3.4315	2.0781	2.7274	4.1579	3.79	2.8945	3.2907
b _T	595.73	722.009	1192.23	908.401	595.871	653.713	855.959	752.901
Kt (L/g)	2.778	12.648	2492.397	101.286	1.639	5.011	97.115	19.31
R ²	0.9702	0.9946	0.8611	0.9327	0.9325	0.988	0.9696	0.9805
Dubin-Raduskevich Isotherm model								
q _m (mg/g)	20.357	20.953	22.314	21.445	17.95	20.001	22.461	21.096
E (kJ/mol)	0.224	0.3536	1.291	0.707	0.224	0.289	0.7071	0.408
R ²	0.9856	0.8529	0.5138	0.6219	0.7165	0.8185	0.7178	0.7597
K (mol ² /J ²)	1*10 ⁻⁵	4*10 ⁻⁶	3*10 ⁻⁷	1*10 ⁻⁶	1*10 ⁻⁵	6*10 ⁻⁶	1*10 ⁻⁶	3*10 ⁻⁶

Rhodamine-B dye standard calibration curve was obtained by recording the absorbance values of various concentrations of Rhodamine-B dye at the maximum absorbance of wavelength 543 nm.

3.1. Adsorbate

Rhodamine-B dye [chemical formula $C_{28}H_{31}ClN_2O_3$, MW 479.01]. The stock solution (1000 ppm) of Rhodamine-B dye is prepared by dissolving 1gm of RhB in 1000 ml of double distilled water.

3.2. Adsorption Studies

Adsorption experiments were performed at room temperature of 25 °C, 100 ml of 50 ppm concentration RhB dye and solution pH maintained natural, as well as desired when needed likewise the other parameters such as adsorbent doses, temperature, and contact time were also either varied or kept at the desired level as per the need. All sample solution was filtered through Goch. The pH of the dye solution was adjusted by using 0.1 M of NaOH or HCl solution. Experiments were carried out twice and the concentrations given were average values. The equilibrium concentrations of RhB dye after adsorption was measured by UV spectrophotometer.

The percentage removal of RB dye was calculated by the following equation

$$\%R = [(C_o - C_e) / C_o] * 100$$

The amount of RB dye adsorbed per unit mass of the adsorbent was evaluated by using the following equation, q_e (mg/g)

$$q_e = (C_o - C_e) / m \cdot V$$

Where C_o = Initial concentration of dye (mg/l)

C_e = the equilibrium concentration (mg/l)

V = the volume of dye solution (L)

m = the mass of adsorbent (g)

4. Results and Discussion

4.1. FTIR analysis of Alum and Mud Sludge Adsorbents and dye loaded Adsorbent

To confirm the adsorption of RhB dye on AS

and MS adsorbents, FTIR spectra was applied for both the developed sludge adsorbents (AS & MS) and dye loaded adsorbents. The FT-IR spectra of the samples were recorded through an FTIR spectrometer using KBr tablets (JASCO 3600Tokyo, Japan) at room temperature in the range 400–4000 cm^{-1} .

4.1.1. FTIR analysis of Alum Sludge adsorbent (AS) and dye loaded adsorbents.

The FTIR spectra of AS adsorbent and dye loaded AS were presented in Fig 1. FTIR spectra of alum sludge adsorbent (AS) showed broadband 1041 cm^{-1} that were assigned to the most intense Si-O stretching modes.

Peaks characteristic broadband appeared at 3433.64 cm^{-1} correspond to the presence of OH stretching vibration due to the extinction of surface hydroxyl group and chemisorbed H_2O , while the absorption band present at 2929-2972 cm^{-1} may suggest the presence of organic carbon. These bands are due to C-H absorption contaminants present in the sample. It can be inferred that the alkane groups do play a significant role in adsorption as their adsorption peak 2929.34 cm^{-1} characteristic of carbon-and hydrogen containing species, with double bond and are assigned to various forms of C-H stretching, and CH_2 alkene. The presence of quartz in the samples the observation of the peaks in the ranges 463 - 465 and 529 - 533 cm^{-1} . Calcite is the most common carbonate mineral in natural samples the existence of peak at 1425 cm^{-1} . The peaks at 460-465 cm^{-1} indicate the presence of microcline. After RhB dye adsorption, peak shifted to 2972.73 cm^{-1} , while peak at 2364.3 cm^{-1} characteristic of carbon-and hydrogen containing species with single bond and are assigned to various forms of C-H stretching. Also, dye loaded AS shifted to 2372.73 cm^{-1} . The presences of these groups are responsible for adsorption of RhB dye onto the Alum Sludge adsorbent, AS, surface.

4.1.2. FTIR analysis of Mud Sludge adsorbent (MS) and dye loaded adsorbent.

FT-IR spectrum of Mud Sludge adsorbent (MS) in Fig (2) which showed a wide band with maximum peak at 3438.46, 3432.67 cm^{-1} . This band can be assigned to the O-H stretching mode of hydroxyl groups and adsorbed water.

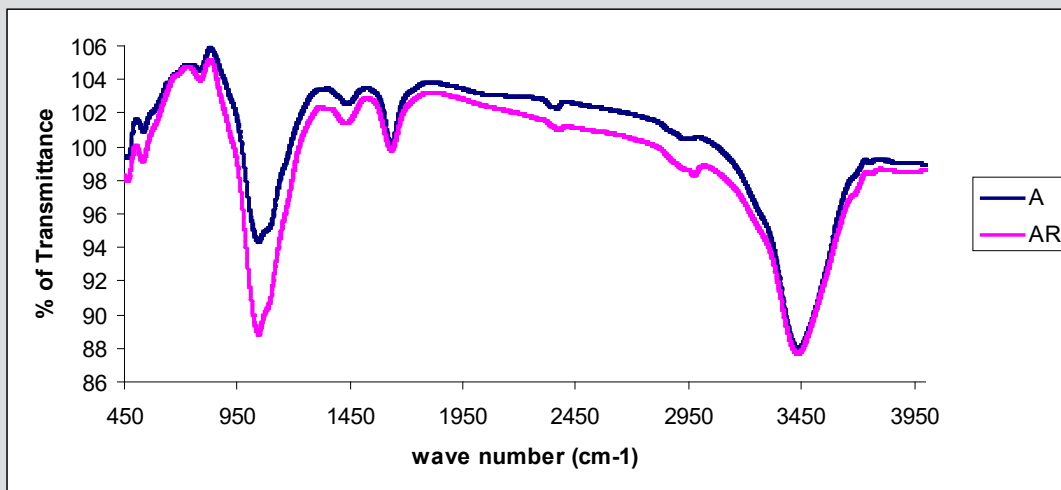


Fig.1. FTIR analysis of alum sludge adsorbent (A) and Rhodamine B dye loaded A (AR)

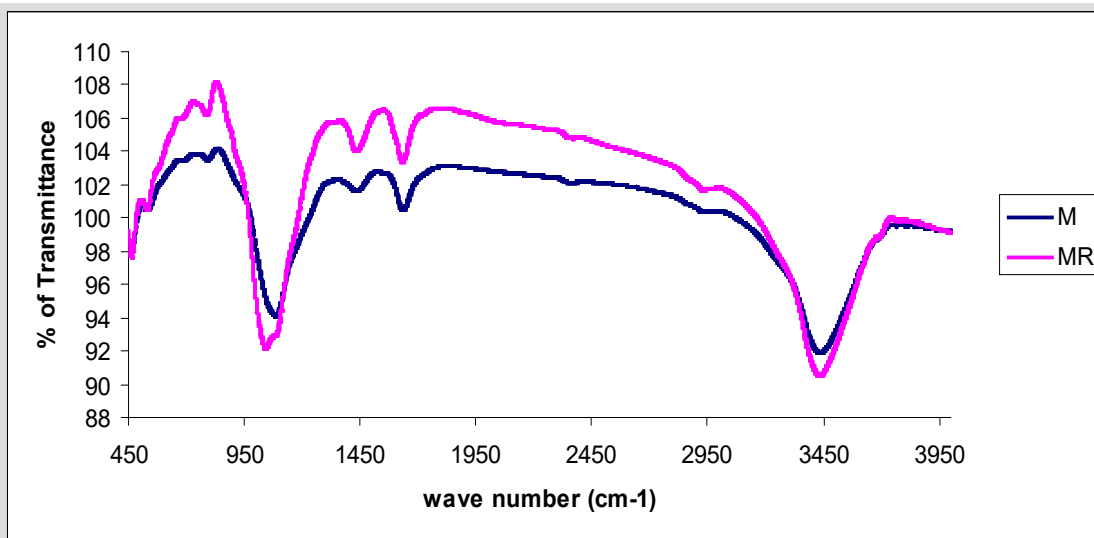


Fig.2. FTIR analysis of mud sludge adsorbent (M) and Rhodamine B dye loaded M (MR)

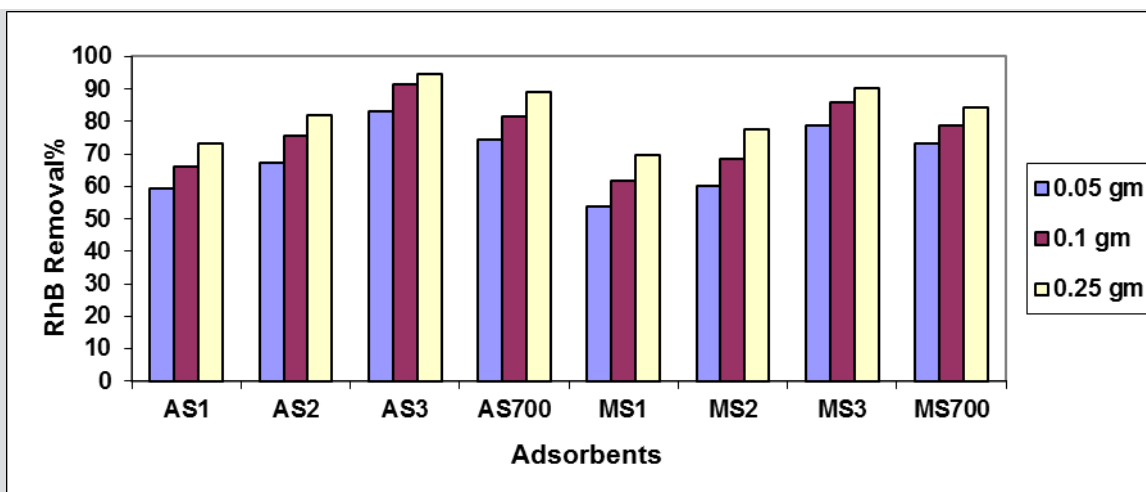


Figure (3). Effect of Alum and Mud adsorbent dosage on RB dye removal.

Broadband at (1041 cm^{-1} and 1085 cm^{-1}) were assigned to the most intense Si-O stretching modes.

The peaks at, 785.85-789.707 cm^{-1} are observed for albite. The observation of the peak in the range 531.29 cm^{-1} indicates the presence of albite ($\text{NaAlSi}_3\text{O}_8$; Na- feldspar) mineral absorption band present at 2928.33 cm^{-1} may suggest the presence of organic carbon. These bands are due to C-H present in the samples. The presence of quartz in the samples is indicated by the observation of the peaks at 461.86 and 465.72 cm^{-1} due to Si-O asymmetrical bending vibrations. After RhB dye adsorption, peak shifted to 2972.73 cm^{-1} . While peak at 2364.3 cm^{-1} characteristic of carbon and hydrogen containing species with single bond and are assigned to various forms of C-H stretching. Also, dye loaded AS shifted to 2372.73 cm^{-1} . The presences of these groups are responsible for adsorption of RhB dye onto the Alum Sludge adsorbent, AS, surface. The presences of these groups are responsible for adsorption of RhB dye on to the Mud Sludge adsorbent (MS).

4.2.A Comparative Study Between the Developed Adsorbents for RB Removal:

The chemical activation of alum and mud sludge (Table 2) shows that the removal percent of RB by adsorbent activated with acetic acid followed by pyrolysis at 500 °C was the best at 3 M acetic acid (72.2%) for Alum Sludge adsorbent (AS1) and 69.6% for Mud Sludge adsorbent (MS1) at 0.1 M of acetic acid. Adsorbents of chemically activated with acetic acid only revealed the highest removal percent of RB (80.6%) for Alum Sludge (AS2) at 0.1 M acetic acid, and 77.8% of Mud Sludge (MS2) at 0.5 M of acetic acid (Table 2). The removal efficiency of RB with adsorbent activated with nitric acid (Table 3) shows highest efficiency (95.2% of Alum sludge, AS3, and 92% of Mud Sludge, MS3) at 0.25 M nitric acid concentration. In the physical activation of the sludge (Table 4) the pyrolysis at 700 °C show the highest removal efficiency of Rh-B (87.8%) for alum sludge adsorbent (AS700) and 83.7% of mud sludge adsorbent (MS700). So, the developed adsorbents AS1, AS2, AS3, MS1, MS2, and MS3 were selected as the most chemically activated sludge adsorbents, while AS700 and MS700 adsorbents as the most

physically activated sludge adsorbents, and will be used in batch adsorption experiments.

4.3. Batch Adsorption and Optimization Conditions.

After selecting the alum sludge adsorbents (AS1, AS2, AS3, and AS700), and the mud sludge adsorbents (MS1, MS2, MS3, and MS700) as the best chemically and physically adsorbents, the following batch adsorption results of RB dye were discussed to determine the optimum condition for RB dye adsorption.

4.3.1. Effect of initial RB dye concentration

The study of the optimum RB dye initial concentration is studied by varying the dye concentration from 50-60-75-100 ppm, while keeping the temperature, adsorbent dose, pH, and contact time constant at 25°C, 0.25 gm, pH 7 and 90 min, respectively. The effect of initial RB dye concentration on the removal efficiency by the adsorbents (AS, MS) is indicated in Table (5). The data evidenced that the RB removal percentage decreases with increasing dye concentration, however, the actual amount of the dye is increased. This is due to increase in dye concentration, surface area and active sites of the adsorbent were saturated and hence percentage removal decreases.

Ilyaraja et al. (2013) found that the percentage removal of RB dye using activated carbon decreased from 86.9% to 52.8% with an increase in concentration of dye from 20 – 100 mg/l. Wang et al. (2016) reported that the removal percentage of RB dye on modified zeolites decreased from 93% to 85% with the increase of initial dye concentration which the adsorption capacity of RB increased. Akash (2013) found that the percentage of removal of RB dye on activated Mahua seed carbon (AMC) and activated neem seed carbon (ANC) decreased with the increase of dye concentration (50-100-150) ppm from 92% to 83% to AMC and from 82% to 64% to ANC.

4.3.2. Effect of adsorbent dosage

In these experiments, target RB dye solutions with a concentration of 50 ppm were placed in contact with various amounts of adsorbent (0.05, 0.1 and 0.25 gm), keeping other parameter (pH,

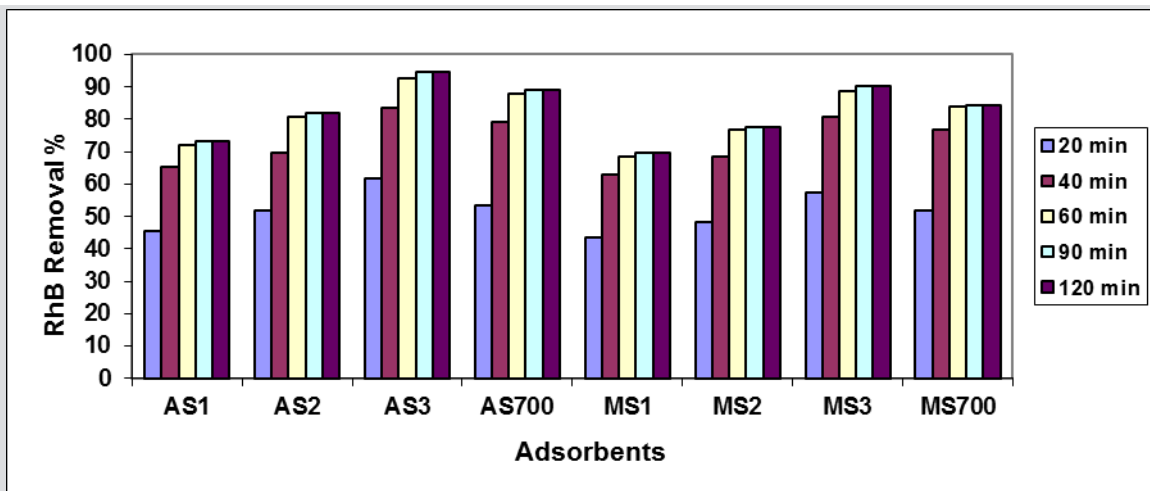


Figure (4). Effect of Alum and Mud adsorbent contact time on RB dye removal.

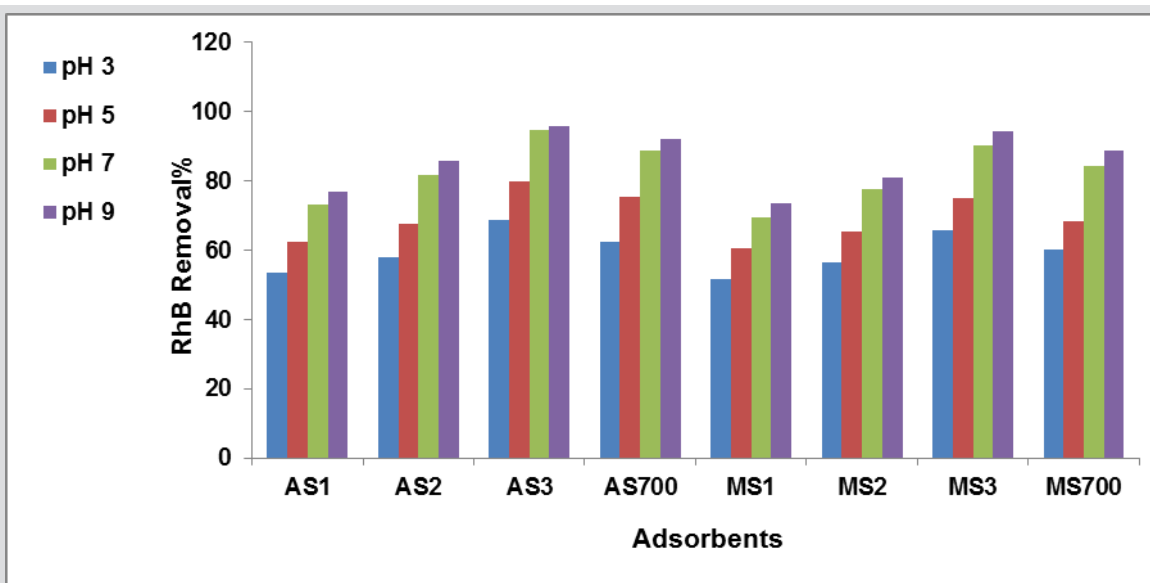


Figure (5). Effect of Alum and Mud adsorbent pH on RB dye removal.

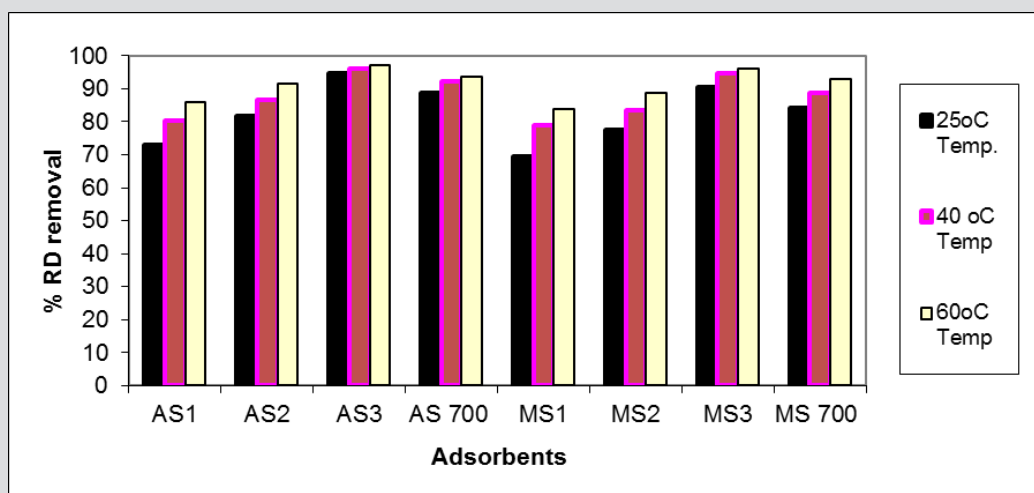


Figure (6). Effect of Alum and Mud adsorbent temperature on RB dye removal.

contact time and temp.) constant. The results are presented in Fig (3) which show that the removal percentage of RB dye increase with increasing adsorbent dose (Alum and Mud) and reached high removal efficiencies with 0.25 gm adsorbent; this because of the number of available adsorption site increases by an increase in adsorbent dose.

Danitel and Shoba (2015), they found that the removal percentage of RD dye adsorbed increase along with the increase of adsorbent dosage of carbon from 50 to 150 mg/l. Ilayaraja et al (2013) found that the removal percentage of RB dye increased with increasing the MAC sorbent dose (maranta arundinacea activated carbon) due to the availability of higher number of adsorbing active sites. This increase was from 88.6 to 92.1% with increase dose from 0.2 to 1.0 gm. A similar result was reported for adsorption of RB on magnesium oxide.

Wang–Yu et al (2016) reported that the removal percentage of Rhodamine B using modified zeolites increased ,when the volume and concentration of the solution were fixed,with the increase of the dosage of the modified zeolites. The free active sites which were employed on the adsorbent increased and the unit adsorbing capacity of Rhodamine B in the solution using modified zeolites decreased . Amina et al.(2015) reported that with increase activated carbon prepared from the sewage sludge dose to 5gm , induces RB dye removal higher than 90%. Daniela et al. (2008) found that the percent of the RD dye removal increase with the increasing of the sawdust doses, due to the higher number of available sorption sites. Balasubramani and Sivara (2014) concluded that the percentage of RB dye sorbed increased as the sorbent dose was increased over the rang 1-3 gm. The adsorption of the RB dye increased from 60 to 70 % with the increase in sorbent dose. This is due to the increase in dosage increase the availability of active sites to the dye molecules.

4.3.3. Effect of contact time on RB dye adsorption

In order to determine the optimum contact time for RB dye removal, its value was varied in the range of (20-40-60-90-120 min) in a series of experiments in which the initial dye concentration, the temperature, pH and adsorbent dose were kept constant at 50 ppm, 25°C, pH 7 and 0.25gm

, respectively. The effect of contact time on RB dye removal of by Alum and Mud sludge adsorbents are indicated in Fig. (4).

The results from Fig. (4) showed that the removal percentage of RB dye with Alum and Mud adsorbents increased with increasing contact time from 20 to 90 min after that it remain constant up to120 min. So that the 90 min as contact time was enough to achieve maximum adsorption of RB on the surface of Alum and Mud adsorbents .

The removal percentage of RB on AS1,AS2, AS3 and AS4 adsorbents increase from 45.5% to73.09 , 51.68% to 81.78% , 61.79 % to 94.57% and 53.3% to 88.91%, respectively as contact time increased from 20 to 90 min. While the removal of RB by MS1, MS2, MS3 and MS4 adsorbents increase from 43,36% to 69.55 ,48.27% to 77.58 ,57.23% to 90.45% and 51.77 to 84.23% , respectively as contact time increased from 20 to 90 min. The qt was increased with the increase of time for all samples up to 90 min, this explained that nearly after 90 minutes qe equilibrium reached and RB dye removal also become constant. So the optimal contact time for RB dye adsorption on the developed adsorbents was 90 minute .This optimal time period was the sufficient time for stabilization of this adsorbent and adsorbate dispersed solution.

Balasubramani and Sivarajaskar (2014) found that the percentage of removal of RB dye increase with increase time the equilibrium time was 3 hours for adsorption RB dye on activated carbon (coconut shell activated carbon). Akash and Arvind (2013) reported that nearly after 180 minutes the qe equilibrium reached and percentage removal of RB dye on AMC(activated Mahua seed carbon) also become constant , so that the optimal contact time of adsorbent the RB dye on AMC was 180 min. This time was the sufficient time for stabilization of this adsorbent. Ilayaraja et al. (2013) studied the equilibrium time for the adsorption of RB dye on MAC (Maranta arundinacea activated carbon) from 20 to 140 min.The optimum time removal was found to be 40min. The removal percentage of RB dye increased from 88.6% to 91.3% from 20 to 40min then remain constant. Daniel and Shoba (2015) observed that the uptake of the RB dye increases with time, and the extent of adsorption is rapid in

the initial stage and become slow in later stage till saturation is attained around 2 hours . This shows that equilibrium can be assumed to be achieved by 2 hours of contact time

4.3.4. Effect of pH

The pH of the dye solution plays an important role in the whole adsorption process. The effect of solution pH of the RB dye adsorption on Alum and Mud sludge adsorbents were determined at pH (3, 5, 7 and 9) with a fixed adsorbent dose of 0.25 mg/100 ml RB dye concentration 50 ppm at 25° C and contact time 90 min. The solution pH was controlled by the addition of 0.1 M HCl or 0.1 NaOH. The results showed in Fig. (5) pointed out that the removal percentage of RB increased with increasing pH from 3 to 9. In case of alum sludge adsorbent, removal percentage increased for AS1 (from 53.6 to 76.8 %) , AS2 (from 58 to 86%) , AS3 (from 68.7 to 96%) and AS4 (from 62.5 to 91.98%) , while with Mud sludge adsorbent RB dye removal were increased for MS1 (from 51.6 to 73.5%) , MS2 (from 56.4 to 80.89%) , MS3 (from 65.7 to 94.5%) , and MS4 (from 60.33 to 88.7%) .At that solution pH the adsorbent surface negatively charged and favors uptake of cationic dyes due to increased electrostatic force of attraction.

A similar result was reported by Balasubbr and Sivarajasekar (2014) who found that the removal percentage of RB dye on coconut shell activated carbon increased with increased pH from 2 to 9. They studied the effect of pH on RB dye adsorption on the activated carbon and found that the dye removal was maximum at acidic condition (<7). The reason for this behavior is due to that the RB molecules are positively charged, and as the initial pH of the test solution increased, the number of negatively charged adsorbent sites increased and positively charged adsorbent sites decreased, which favors the adsorption of positively charged dye cation due to electrostatic attraction. Thus at higher pH adsorption will be more and lower pH adsorption will be lesser . Nity et al. (2008) found that the effect of pH on the percentage removal of the RB dye by activated carbon increased with increasing pH from 3 to 7 , and above pH 7.5 removal of RB decrease with increase in pH . Gurusamy et al.(2002) studied the effect of solution pH on the adsorption of dyes (MO,MB,RB,CR,MV and AV

) by banana and orange peels found that ,the amount of adsorption increases when the pH is increased . The adsorption capacities reach maximum at pH 6-7 but decreased when pH is increased further .

4.3.5. Effect of temperature

The effect of temperature on the adsorption of RB on Alum and Mud sludge adsorbents has been studied with different solution temperature (25°C, 40°C, 60°C). The experiment was performed at adsorbent dose 0.25 gm, target dye concentration 50 ppm, contact time 90 min and pH 7. The results are represented in Fig. (6), It showed that the removal percentage of RB dye on Alum and Mud sludge increased with increasing the temperature from 25 °C to 60 °C. The equilibrium of RB adsorption capacity of both adsorbents (AS and MS) were better at higher temperatures as the adsorbed amount of RB increases with the rise in temperature . Higher RB uptake at high temperature is due to the increase in molecular diffusion or may be attributed to the availability of more active sites on surface area. This result indicated that the adsorption of RB dye was an endothermic process.

Similar results have been reported for the adsorption of RB dye by Ilayaraja, et al.(2013) and showed that the adsorption of both CR and RB on MAC is favored by an increase in temperature. Akash and Arvind (2013) reported that the adsorption capacity of RB dye on AMC increases with increase temperature from 35 °C to 65 °C. Daniela et al.(2008) found that the removal percentage of all dyes (MB, CV, RB and B red) on sawdust are greater at increase the temperature the sorption process is an endothermic.

4.4. Adsorption Isotherms

The experimental data collected at 25°C , initial dye concentration 50 ppm , 0.25gm of sludge adsorbent , and 90 min. The data were fitted into the following isotherms: Langmuir, Freundlich, Temkine and Dubinin-Raduskevich (D-R) isotherm models.

4.4.1. Langmuir isotherm:

The Langmuir model assumes that the solid surface carries a limited number of sites that are

characterized by equal energy of adsorption, independent of the degree of coverage and thus indicating a monolayer adsorption. The linearized form of Langmuir equation is described by equation:

$$C_e/q_e = 1/Q_0 b_l + C_e/Q_0$$

Where C_e is the equilibrium concentration of dye solution (mg/l), q_e the equilibrium capacity of dye on adsorbent (mg/g), Q_0 is monolayer adsorption capacity of adsorbent (mg/g) and b_l is the Langmuir bonding energy coefficient (L/mg).

The b_l and Q_0 can be calculated from the intercept and slope of the linear plot of C_e/q_e against C_e .

From data in Table (6), $R^2 = 0.99$ and b_l values lies between 0 to 1 and indicating the favorable sorption of RB dye on both Alum and Mud sludge adsorbents . Therefore , monolayer coverage of RB on Alum and Mud sludge adsorbent particles is assumed with the maximum adsorption capacity of 23.36 mg/g for AS1 , 24.09 mg/g for AS2 , 25.64 mg/g for AS3 , and 24.69 mg/g for AS4 for Alum sludge adsorbent , while for Mud sludge adsorbent it were 22.72 mg/g for MS1 , 23.69 mg/g for MS2 , 25.70 mg/g for MS3 and 27.55 mg/g for MS4. The RB sorption data on both AS and MS adsorbents fitted well to langmuir isotherm model.

4.4.2. Freundlich isotherm:

The Freundlich equation is used to determine the applicability of heterogeneous surface energy in the adsorption process. The empirical Freundlich equation is expressed as:

$$\log q_e = \log K_f + 1/n \log C_e$$

Where K_f is the Freundlich isotherm constants indicating the adsorption capacity, and n is the adsorption intensity. If the $1/n$ values are below one it indicates a normal adsorption , on the other hand $1/n$ being above one indicates cooperation adsorption . The K_f and n can be calculated from the intercept and slope of the linear plot of $\log q_e$ against $\log C_e$. The values of K_f and $1/n$ given in the Table 6 which indicate an effective adsorption. It also indicates the degree of adsorption favorability of. Higher values of k_f indicate higher affinity for RB adsorption.

From the results of Langmuir and Freundlich data it was clearly observed that both models were well suited for adsorption of RB dye on AS and MS adsorbents, but the regression factor as well as the calculated and experimental values correlated more correctly with the langmuir values, on this basis it could be concluded that RB form monolayer on surface of sludge.

4.4.3. The Temkin Isotherm:

The Temkin isotherm model predicts a uniform distribution of binding energies over the population of surface binding adsorption. Linear form of Temkin equation is expressed as:

$$q_e = B \ln K + B \ln C_e$$

Where B is RT/b , and b is the Temkin constant related to heat of sorption . q_e (mg/g) and C_e (mg/l) are the amount of adsorbed dye per unite weight of adsorbent and unadsorbed dye concentration in solution at equilibrium, respectively. Therefore, a plot of q_e versus $\ln C_e$ enables one to determine the constant B that is the constant related to the heat of sorption (J/mol), and K is the equilibrium binding constant (Table 6).

4.4.4. Dubinin- Radushkevich isotherm model:

Dubinin- Radushkevich isotherm is applied to express the adsorption mechanism with a Gaussian energy distribution onto a heterogeneous surface (Gunay and Arslankaya, 2007 ; Dabrowski, 2001) . It means that it is applied to distinguish between physical and chemical adsorption of dye.

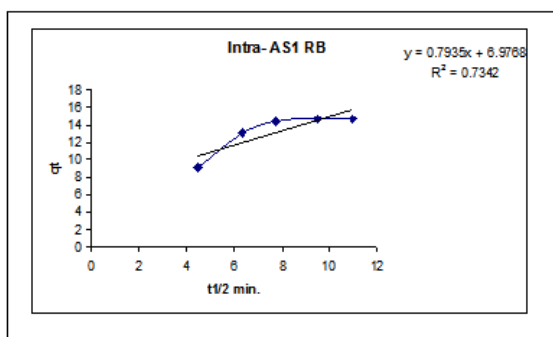
The linearized D-R equation (Chen, et.al, 2008) may be written as:

$$\ln q_e = \ln q_m - BE^2$$

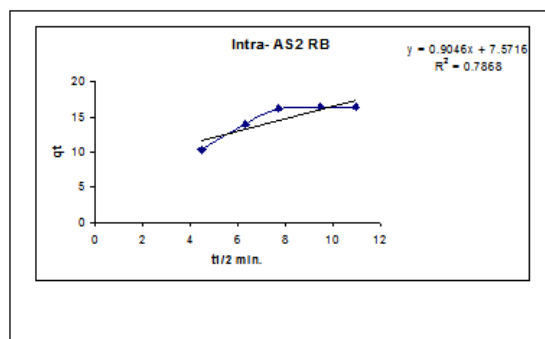
Where B a constant related to the adsorption energy (mol^2/kJ^2), q_m is a constant that indicates the sorption degree characterizing the sorbent (mg/g), and E is the polany potential, which can be obtained by following equation:

$$E = RT \ln (1+1/C_e)$$

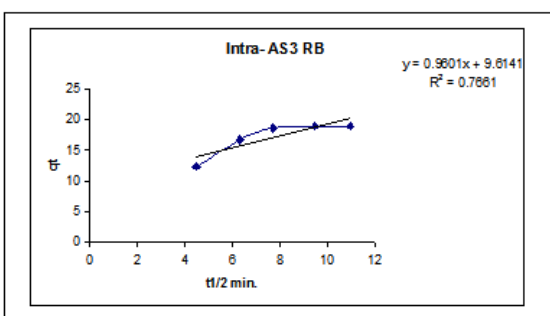
Where R is the ideal gas constant ($R=8.314 \text{ J/mol K}$) and T is the absolute temperature (K). By plotting $\ln q_e$ vs E^2 , it is possible to determine



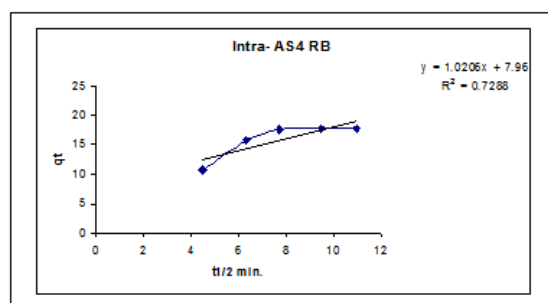
(A) AS1



(B) AS2

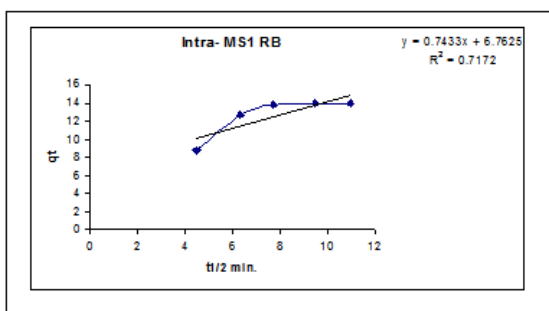


(C) AS3

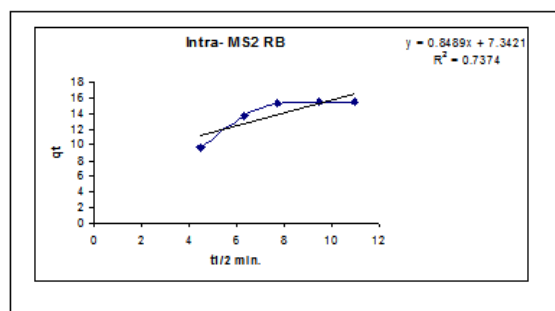


(D) AS700

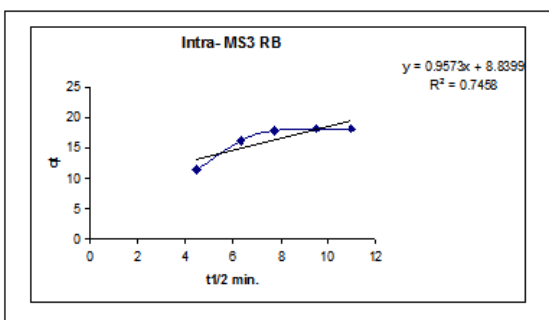
Figure (7). The intra-particle kinetic for the adsorption of RB by AS adsorbents.



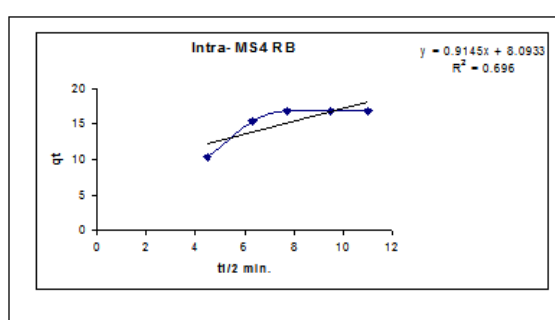
(A) MS1



(B) MS2



(C) MS3



(D) MS700

Figure (8). The intra-particle kinetic for the adsorption of RB by MS adsorbents.

the value of B from the slope and the value of q_m from the intercept, which is $\ln q_m$. The mean free energy E (KJ/mol) of sorption can be estimated by using B values as expressed in the following equation (Chowdhury and Saha, 2010).

$$E = 1/ (2B)^{1/2}$$

The magnitude of E may characterize the type of the adsorption as chemical ion exchange ($E=8-16$ kJ/mol), or physical adsorption ($E < 8$ kJ/mol) (Sivakumar and Rupainwar 2011). From Table (6) it can be observed that the obtained values of the mean free energy are limited within the range of 0.224 to 1.291 kJ/mol. Based on these data, it can thus be concluded that the effect of physical adsorption will play a dominating role in the adsorption process of RB dye adsorption onto the adsorbents. The similar result was reported for adsorption of RB and CR on MAC by Ilayaraja et al. (2013) whom found that the adsorption of RB and CR dyes physical adsorption process. The sorption data fitted into Langmuir, Freundlich, Temkin and Dubunin – Radushkevich isotherms out of which Langmuir Adsorption model was found to have the highest regression value and hence the best fit.

4.5. Adsorption Kinetic Studies:

Kinetic models have been proposed to determine the mechanism of the adsorption process which provides useful data to improve the efficiency of the adsorption and feasibility of process scale-up (Eftekhari et al. 2010). It means to describe the rate of uptake of dyes onto the adsorbents and this rate controls the equilibrium time.

The kinetics adsorption that define the efficiency of RB dye adsorption on Alum and Mud sludge adsorbents were checked by the Pseudo – first order, Pseudo – second order, Intra – particle diffusion and Elovich models. These models include all steps of adsorption which include external film diffusion, internal particle diffusion and adsorption.

4.5.1. Pseudo – first order model

The pseudo- first order kinetic model is represented as follows:

$$\log (q_e -qt) = \log q_e - (k_1/2.303) t$$

Where, q_e and q_t (mg/g) are the sorption capacities at equilibrium and time (min) respectively, and k_1 is the rate constant of the pseudo- first order (Kamal et al.,2010) ; Inbaraj and Sulochana,2005).

A plot of $\log (q_e-qt)$ vs t should give linear relationship with the slope k_1 and intercept of $\log q_e$ the data showed in Table 7. The kinetic parameters and the correlation coefficients for adsorption of RB dye on Alum and Mud sludge adsorbents are presented in Table 7.

4.5.2. Pseudo – second order model:

The linearized form of the pseudo – second order kinetic model is represented as:

$$t/qt = 1/k_2q_e^2 + 1/q_e t$$

Where k_2 is the rate constant of pseudo – second order adsorption (g/mg/min).

A plot of t/qt vs t shows a linear relationship values of k_2 and equilibrium adsorption capacity q_e were calculated from intercept and slope of the plot. The data in Table(7) shown that the correlation coefficient (R^2) is high for pseudo second order. So that the adsorption of RhB dye by Alum and Mud sludge adsorbents are to follow the pseudo second order kinetic.

4.5.3. Intra-particle diffusion model:

For solid – liquid adsorption process, the solute transfer is usually characterized by intra – particle diffusion model proposed by Weber and Morris (1963) which was used to identify the mechanism involved in the adsorption process:

$$qt = k_i t^{1/2} + C$$

Where, k_i ($\text{mg g}^{-1} \text{min}^{-1/2}$) is the rate constant of the intra-particle diffusion model and C (mg g^{-1}) is intraparticle diffusion constant i.e. intercept of the line (mg g^{-1}). It is directly proportional to the boundary layer thickness, and reflects the boundary layer effect. The k_i and C can be determined from the slope and intercept of the linear plot of qt vs $t^{1/2}$ Figs. (7&8).

The experimental data were used for intraparticle diffusion model(intraparticle diffusion constant [K_{id}], intercept and the correlation coefficient [R^2]) are calculated.

Table 7. Calculated kinetic parameters for the adsorption of Rhodamine B dye onto Alum and Mud sludge adsorbents.

Parameters	AS1	AS2	AS3	AS4	MS1	MS2	MS3	MS4
Pseudo first order								
K_1 (min) ⁻¹	0.0859	0.08153	0.0732	0.0859	0.0804	0.0953	0.0726	0.1048
qe (mg/g)	36.058	39.03	31.989	45.783	28.249	50.119	30.4019	65.494
R ²	0.9752	0.9401	0.9803	0.9789	0.9934	0.955	0.993	0.9695
Pseudo second order								
K_2 (g/mg min)	5.071*10 ⁻³	4.215*10 ⁻³	4.303*10 ⁻³	3.755*10 ⁻³	5.514*10 ⁻³	4.716*10 ⁻³	4.2348*10 ⁻³	4.5095*10 ⁻³
qe (mg/g)	16.393	18.45	21.0084	20.161	15.552	17.422	20.2020	18.868
R ²	0.9934	0.9947	0.996	0.9916	0.9933	0.9932	0.9947	0.9916
Elovich model								
α (mg/min)	3.996	4.235	6.7692	3.967	4.0096	4.1297	5.4429	4.5693
β (g/mg)	0.3247	0.288	0.26996	0.2522	0.3455	0.3037	0.2697	0.2797
R ²	0.8422	0.8826	0.8683	0.8378	0.8278	0.8448	0.8519	0.8097
Intra particle diffusion model								
K_{id}	0.7935	0.9046	0.9601	1.0206	0.7433	0.8489	0.9573	0.9145
C (mg/g)	6.9768	7.5716	9.6141	7.96	6.7625	7.3421	8.8399	8.0933
R ²	0.7342	0.7868	0.7661	0.7288	0.7172	0.7374	0.7458	0.696

Table 8. Thermodynamical parameters for the adsorption of Rhodamine B dye onto Alum and Mud Sludge adsorbents.

Parameters	AS1	As2	As3	As4	MS1	MS2	MS3	MS4	
ΔH^0 , kJ/mol	19.2178	21.1783	15.773	14.1446	18.9983	19.1139	15.2296	20.9621	
ΔS^0 , kJ/K/mol	0.06531	0.07583	0.06928	0.05769	0.06339	0.06687	0.06223	0.07657	
ΔG^0 , kJ/mol	298 k	-0.2438	-1.4189	-4.8729	-3.0463	-0.1081	-0.8132	-3.3163	-1.8571
	313 k	-1.2242	-2.5565	-5.9121	-3.9124	-0.8428	-1.8163	-4.2498	-3.0057
	333 k	-2.5304	-4.0731	-7.2977	-5.0662	-2.111	-3.1536	-5.4945	-4.5372
R ²	0.9968	0.9979	0.9869	0.9701	0.9666	0.9999	0.9991	0.9987	

The intraparticle diffusion plots of 'qt' vs 't^{1/2}' for the adsorption of Rh.B dye on AS and MS adsorbents are shown from in Figures (7&8) and the values are given in Table 7. From the figures (7 &8), the first line would represent fast uptake and rapid transfer of adsorbate Rh.B dye onto the adsorbent surface by physical/chemical forces. The line in the initial stage does not pass through the origin this makes it noteworthy that uptake is dominated by film diffusion than it does for the intraparticle diffusion process. In the second stage, sorbate adsorption speeds up reflecting non consecutive diffusion of sorbate molecules into the micropores with pore width within the sorbent, while the third stage shows saturation of adsorbent surface. High regression coefficient values obtained also indicated a possible role of diffusion within particles during Rh.B sorption. Generally, adsorption controlled by the intraparticle model is due to the preferential adsorption of sorbate in the micropores (Biyan et al., 2009).

From these data the intercept value indicates that the lines are not passing through origin, therefore some other process that may affect the adsorption. The correlation coefficient [R²] value is less than that of pseudo second order model.

4.5.4. Elovich model:

One of the most useful models for describing such adsorption kinetic of activated chemisorptions is Elovich equation.

The Elovich equation was: $qt = 1/\beta \ln[\alpha\beta] + 1/\beta \ln t$

Where, α , the initial adsorption and β , the desorption coefficient

The constant α and β are calculated from plots obtained when qe is plotted vs $\ln t$.

The results are shown in Table (7). The parameters of Elovich kinetic model α , β and correlation coefficient [R²] are summarized in Table (7).

The data obtained from Elovich model (the initial adsorption rate [α], desorption constant [β] and the correlation co-efficient (R²) were calculated and tabulated in Table (7). The correlation coefficient [R²] is less than that of pseudo second order model. The desorption coefficient (β), which

is related to surface coverage, increases with an increase in the initial dye concentration indicating the decrease in availability of adsorption surface for the adsorbate. The constant (α) is an indication of the number of sites available for the adsorption. The correlation coefficient value (R²) is found to be linear indicating favorable

adsorption but the value is less when compared to pseudo second order kinetic model.

Finally from Table (7) it indicates that all these four kinetic models, applied for adsorption of RhB on Alum and Mud sludge adsorbents, are to follow pseudo second order kinetic model.

4.6. Thermodynamics of adsorption:

The thermodynamic parameters such as changes in Gibbs free energy (ΔG^0), enthalpy (ΔH^0) and entropy (ΔS^0) are the actual indicators for particle applications. Adsorption thermodynamics were evaluated with respect to different temperatures (298, 313, and 333 K)

The thermodynamic parameters were calculated by the following equation:

$$\ln k = \Delta S^0 / R - \Delta H^0 / RT$$

Where, R is the gas constant (8.314 J/mol K) and T is temperature (K).

Both ΔH^0 and ΔS^0 were determined from the slope and intercept of the van'tHoff plots of $\ln k$ vs $1/T$ (Ozcan et al., 2006, Nollet et al., 2003) The free energy of specific adsorption ΔG^0 (KJ/mol) is calculated from the following expression.

$$\Delta G^0 = \Delta H^0 - T \Delta S^0$$

The estimated thermodynamic parameters are presented in Table (8). The adsorption data indicate that ΔG^0 values were negative at all temperatures. That negative ΔG^0 confirms the spontaneous nature of adsorption of RhB by alum and mud sludge adsorbents. The parameter ΔG^0 suggests that adsorption of RhB is physical adsorption process. The positive values of ΔH^0 were further confirmed the endothermic nature of adsorption process. The positive ΔS^0 showed increased randomness at the solid – solution interface during the adsorption of RhB by Alum and Mud sludge adsorbents.

Conclusion

The present study shows that Alum and Mud sludge adsorbents are an effective adsorbent for the removal of RhB dye from aqueous solution. The adsorption followed the Langmuir isotherm and pseudo – second order kinetic .

The thermodynamic parameters were found to be thermodynamically favorable physical adsorption process. Evaluation of thermodynamic parameters showed the process as endothermic and spontaneous. Complete removal of the dye can be achieved using an appropriate dosage of the adsorbent and pH 7. The results would be useful for the fabrication and designing of wastewater treatment plants for the removal of RhB dye. Since the raw material is freely available in large quantities the treatment method, seems to be economical.

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